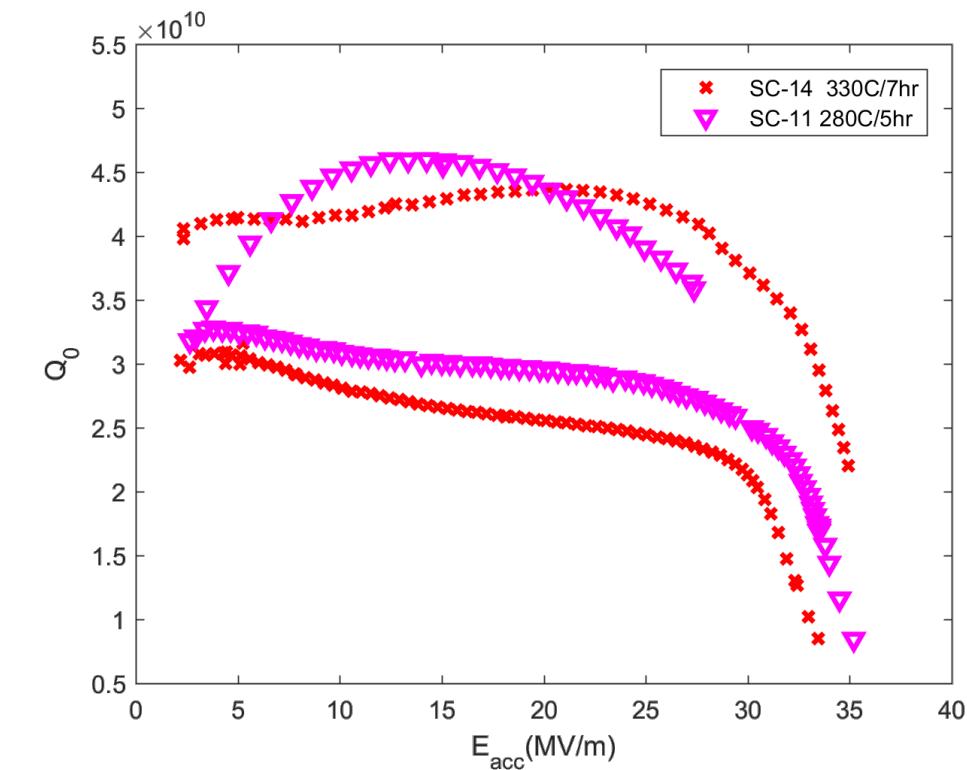
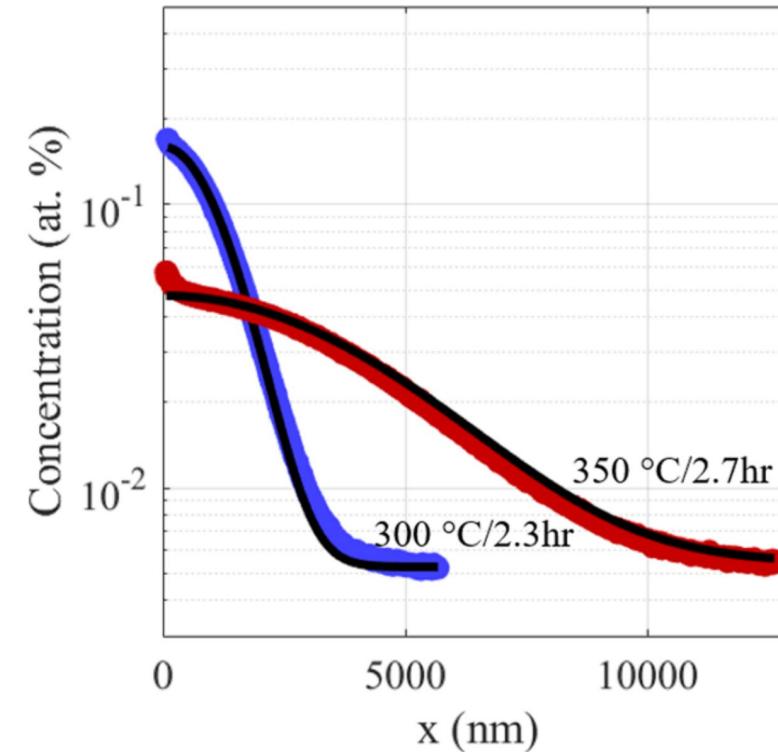
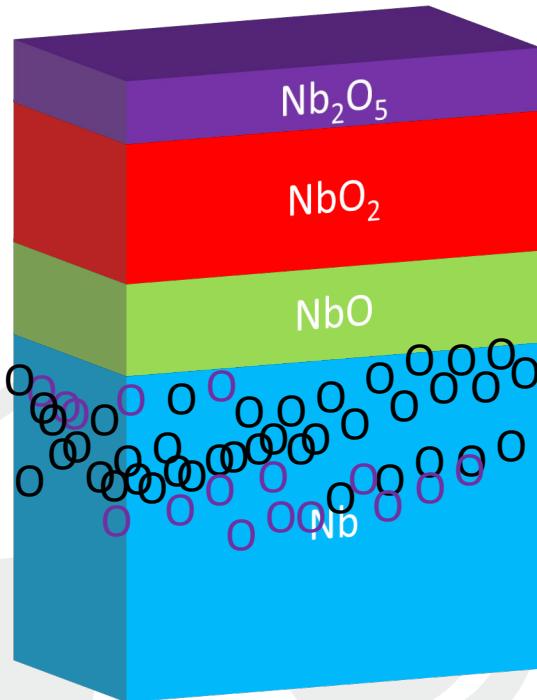


Modeling O Diffusion During Nb Oxide Dissolution



Eric Lechner

Monday, October 10, 2022

Outline

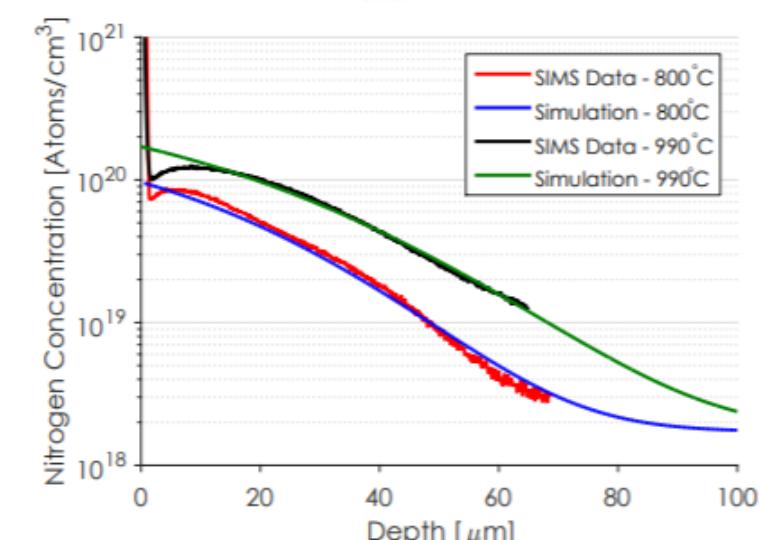
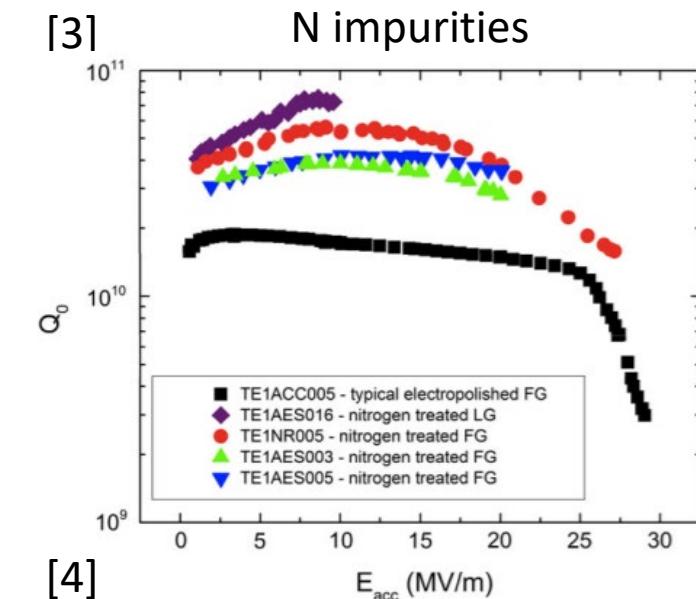
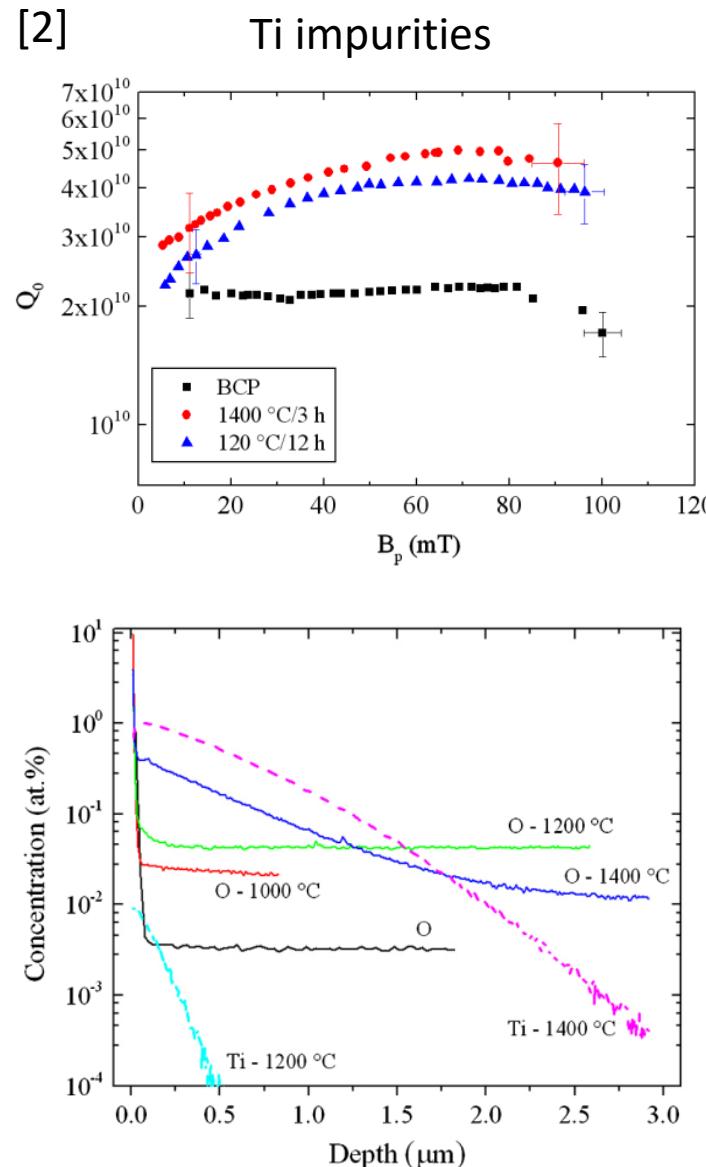
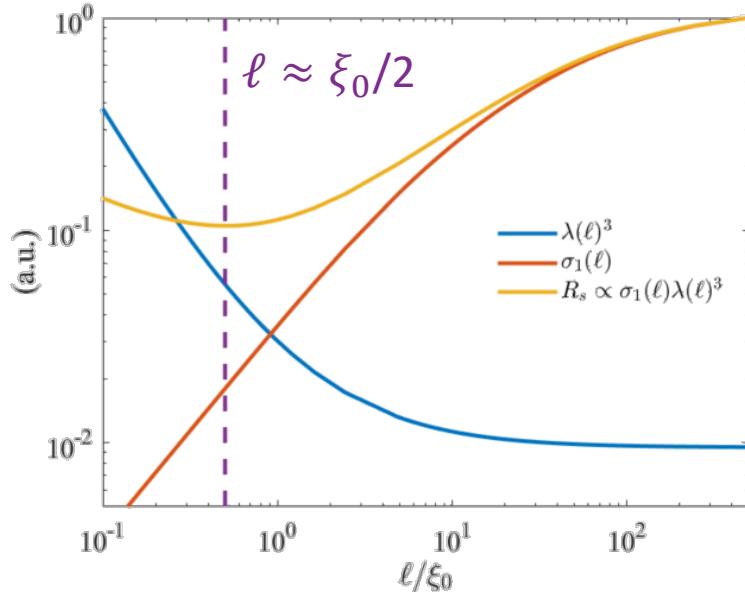
- Motivation
- Modeling O Diffusion
- Where next?

Motivation - Impurity Alloying

Why introduce impurities?

- 2-4 times more efficient
- Only way to obtain high Q_0

Calculated from [1] $R_s = \frac{1}{2} \mu_0^2 \omega^2 \lambda^3 \sigma_1$,



[1] Kubo, Takayuki. *Physical Review Applied* 17.1 (2022): 014018.

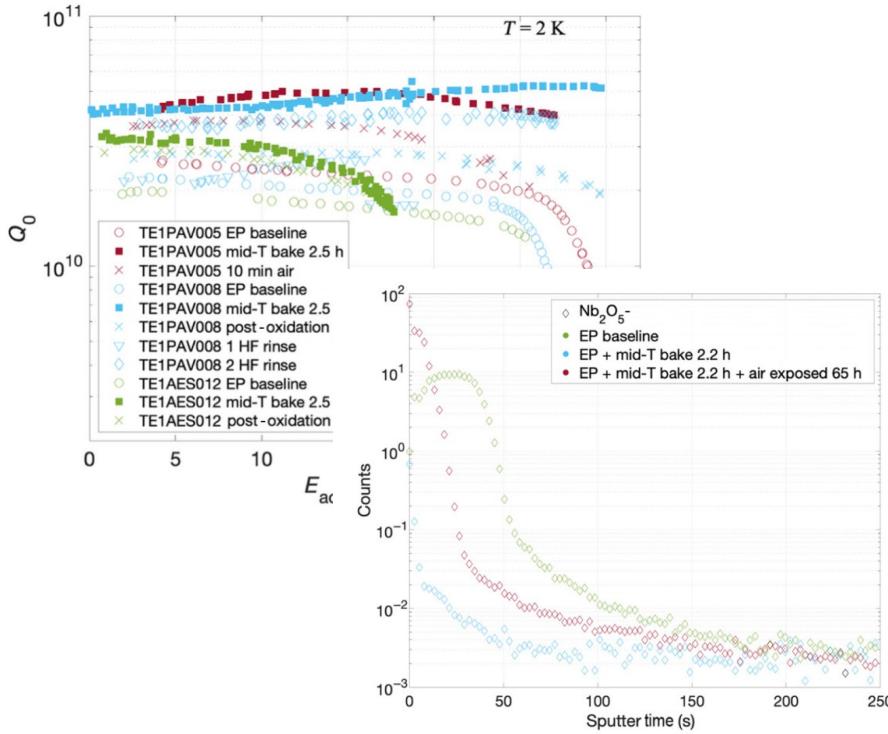
[2] Dhakal, P., et al. *Physical Review Special Topics-Accelerators and Beams* 16.4 (2013): 042001.

[3] A. Grassellino et al. *Supercond. Sci. Technol* 26.10 (2013): 102001.

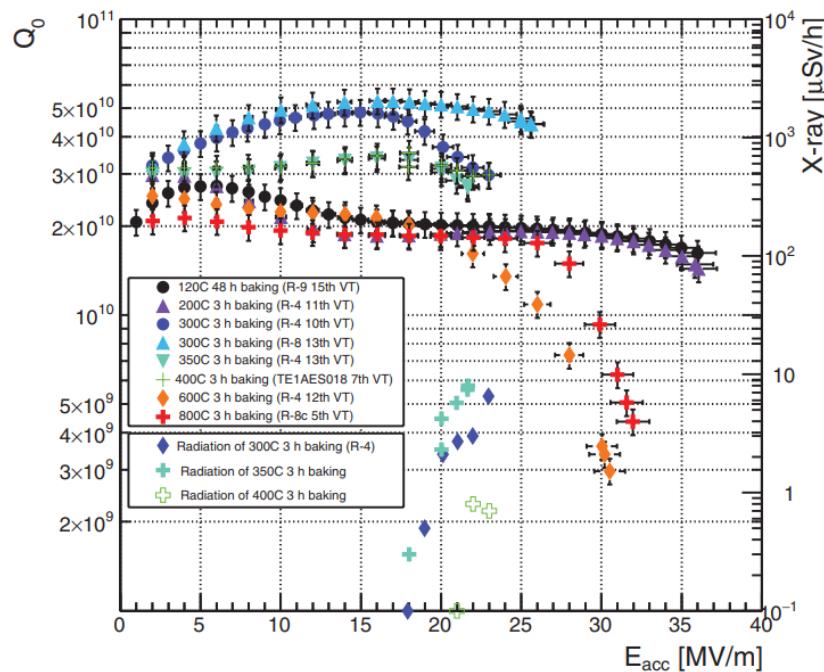
[4] D. Gonnella, Daniel, et al. *Proceedings of IPAC2016, Busan, Korea* (2016).

Recent Experiments

[1]



[2]

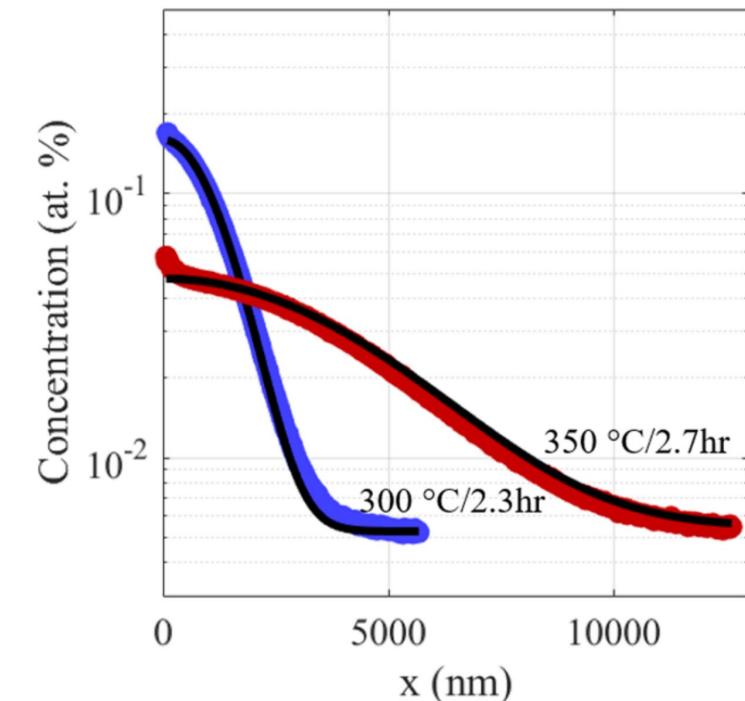


- Efficacy of cavities heat treated at 250-400 C
 - Nb pentoxide dissolution observed

- Cavities heat treated between 200-400 show an enhancement in Q , but at higher temperatures it resembles a baseline cavity
 - Consistent with an alloying agent being introduced and diffused away

[3]

O impurities



- Oxygen shown as major contributor at ~ 0.1 at %. A similar concentration of N in N doped cavities.
- Consistent with Ciovati's model of Nb pentoxide dissolution and O diffusion.

[1] Posen, S., et al. *Physical Review Applied* 13.1 (2020): 014024.

[2] Ito, H., et al. *Progress of Theoretical and Experimental Physics* 2021.7 (2021): 071G01.

[3] Lechner, E. M., et al. *Applied Physics Letters* 119.8 (2021): 082601.

Motivation – Simplified Processing

[1]

O-alloying

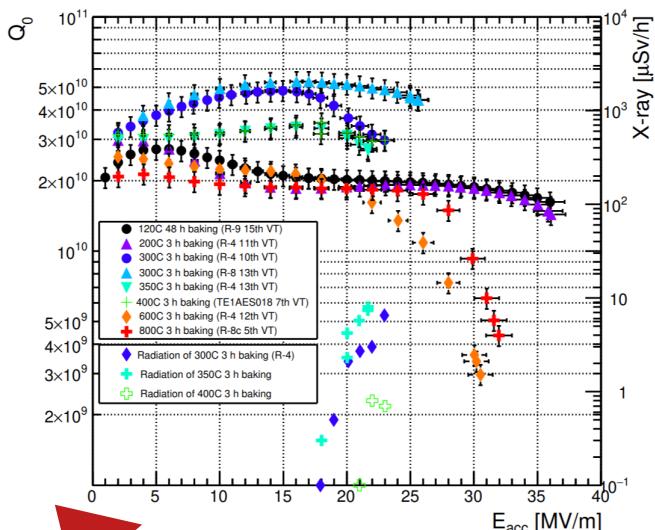
Ito et al.'s cavity prep.

Reset Electropolish

High Pressure Rinse

Vacuum heat treat (200-800 C)

High Pressure Rinse+RF test



[2]

N-doping

High temperature degassing
800 °C (~ 3 hours) in UHV

Nitrogen injection at the end of process (~ 25 mTorr) hold for 'x' mins

Evacuate furnace and temperature hold for 'y' mins

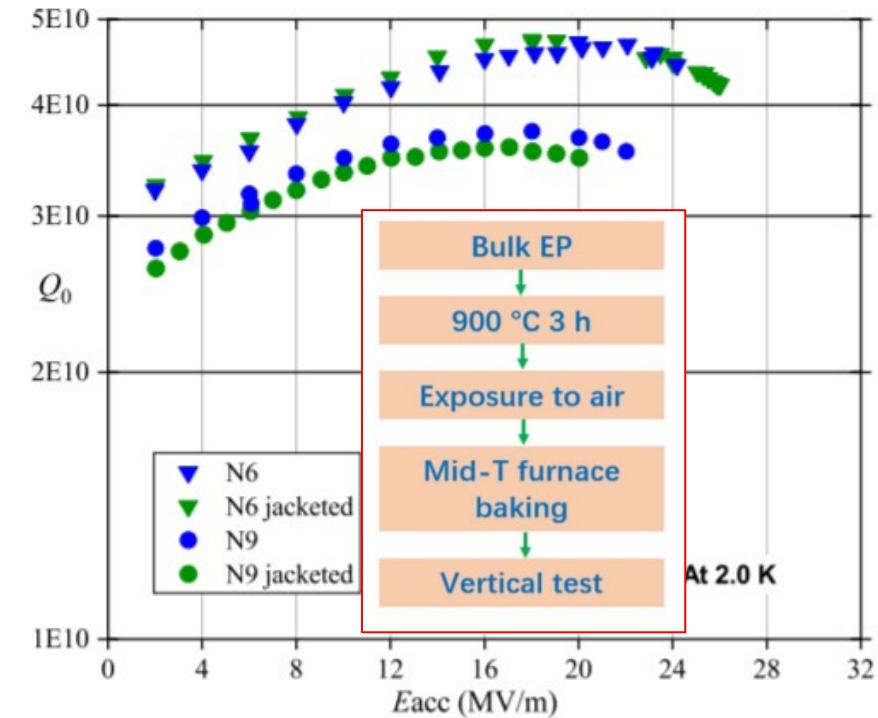
Furnace cooldown to room temperature in UHV

Electropolishing (5-10 μm)

High Pressure Rinse (HPR), clean room assembly and rf test

[3]

How simple can O-alloying get?



COMPLICATED!

SIMPLE!

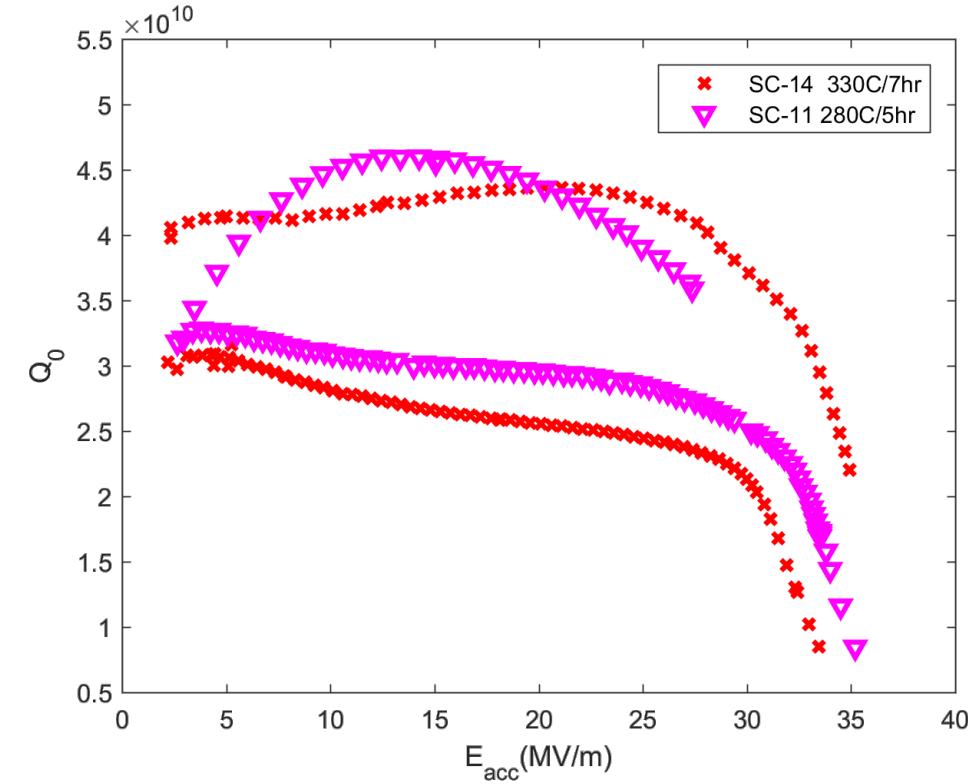
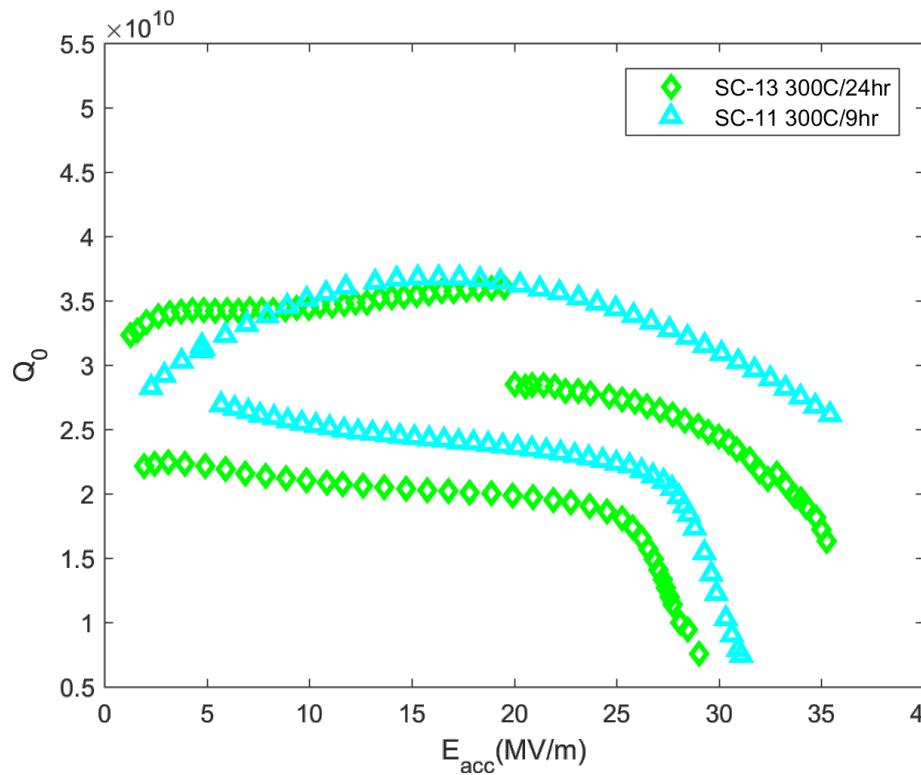
[1] H. Ito et al. Progress of Theoretical and Experimental Physics, 2021;, ptab056

[2] P. Dhakal *Physics Open* (2020): 100034.

[3] F. He, et al. *Superconductor Science and Technology* 34.9 (2021): 095005.

High Q₀ and High E_{acc}

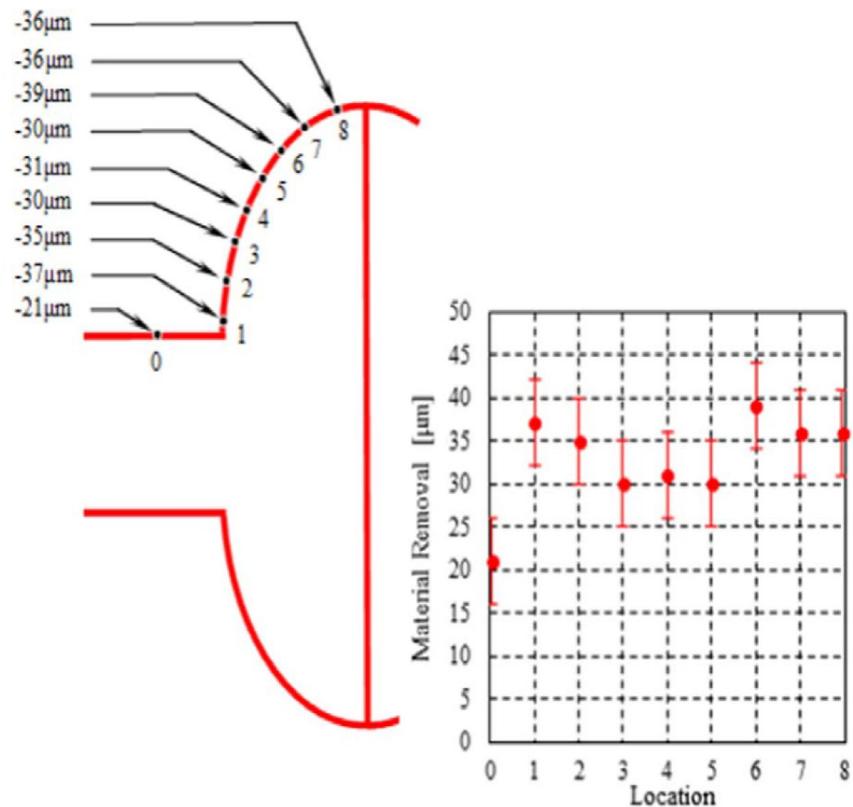
1.3 GHz Single Cell RF Tests



- High Q
- E_{max} that match or exceed the baseline max

Benefits – Conformal

[1]



[2]

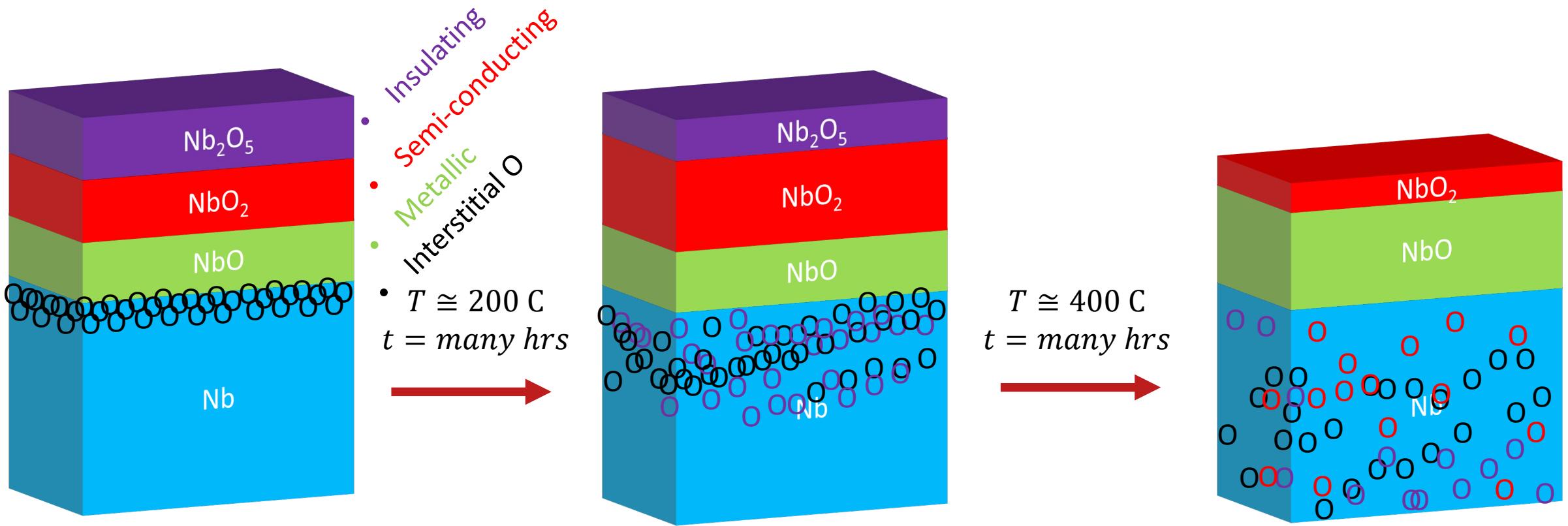


- N-alloying requires an additional electropolishing step to remove lossy nitrides.
- On complicated shapes this may result in non-uniform impurity profiles exposed to the RF surface. No electropolishing required with O-alloying
- The oxygen source is inherently conformal to the cavity shape

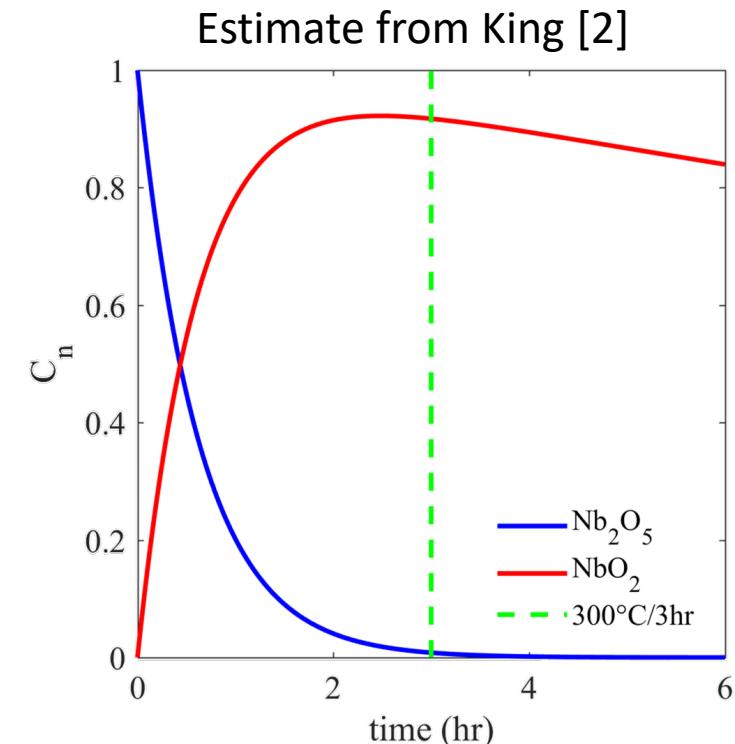
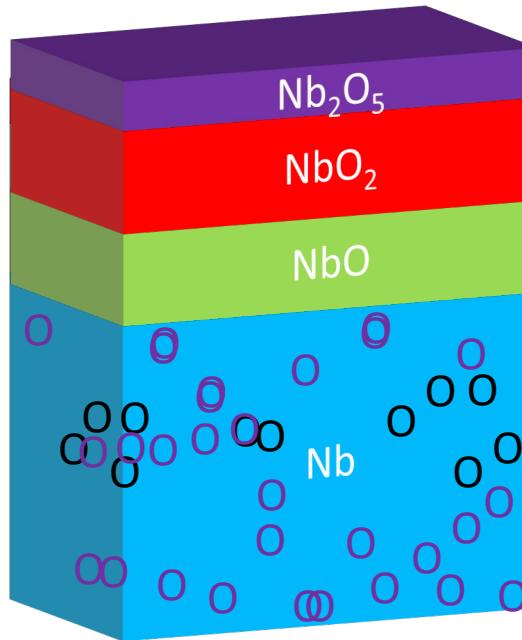
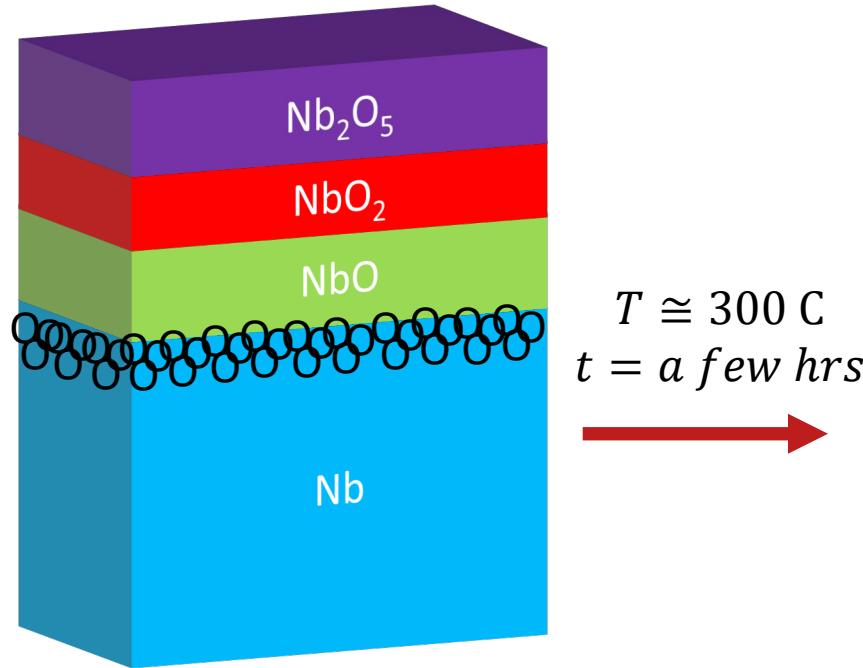
Outline

- Motivation
- Modeling O Diffusion
- Where next?

Native Oxide Dissolution



Ciovati's Native Oxide Dissolution and Diffusion Model



One-dimensional diffusion equation [1]

$$\frac{\partial c(x, t)}{\partial t} = D(T) \frac{\partial^2 c(x, t)}{\partial x^2} + q(x, t, T).$$

$$c(x, t) = v(x, t) + u(x, t)$$

Solutions to the diffusion equation

$$v(x, t) = \frac{v_0}{\sqrt{\pi D(T)t}} e^{-x^2/(4D(T)t)} + c_\infty - \text{superficial dissolved oxygen}$$

$$u(x, t) = \frac{u_0}{\sqrt{\pi D(T)}} \int_0^t \frac{k(T) e^{-k(T)s}}{\sqrt{t-s}} e^{-x^2/(4D(T)(t-s))} ds - \text{oxide dissolution}$$

Arrhenius equations

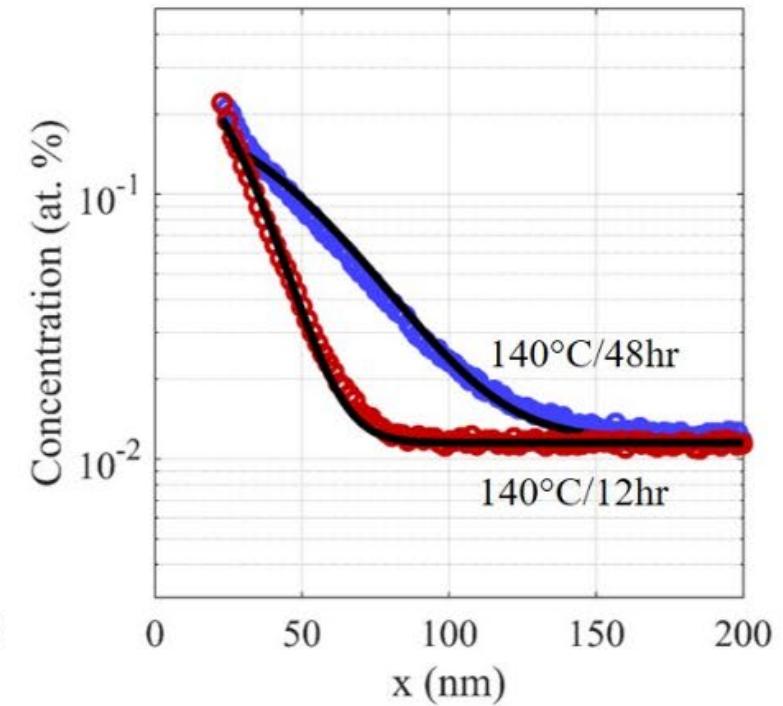
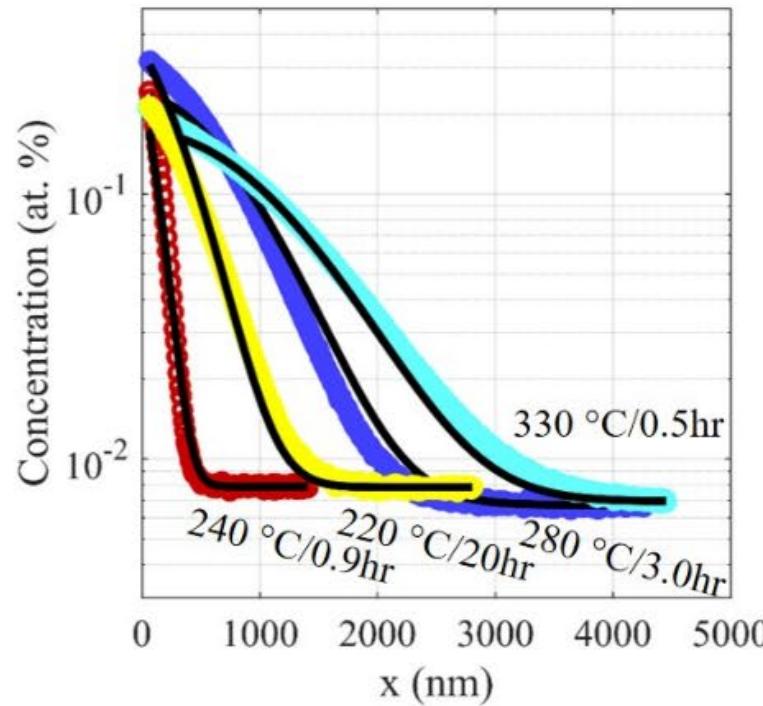
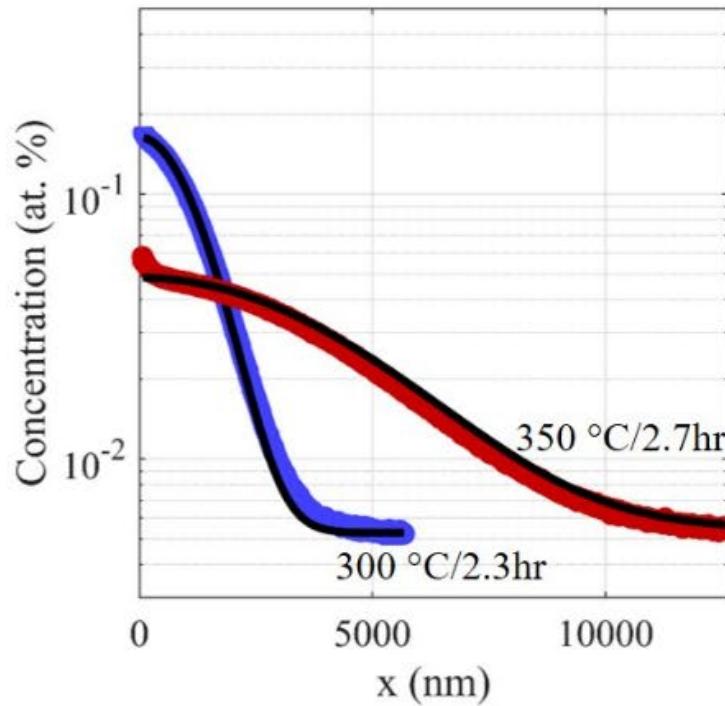
$$D(T) = D_0 e^{-E_{aD}/RT} - \text{oxygen diffusion}$$

$$k(T) = A e^{-E_{ak}/RT} - \text{oxide dissolution}$$

[1] Ciovati, Gianluigi. *Applied physics letters* 89.2 (2006): 022507.

[2] King, B. R., et al. *Thin Solid Films* 192.2 (1990): 351-369.

Application of Ciovati's Model – SIMS O Concentration Depth Profiles



- Measurements are consistent with Ciovati's model
- May be able to tune interstitials by changing only temperature and time of vacuum anneal, but missing components of the slower dioxide dissolution.

superficial dissolved oxygen

$$v_0 = 3.5 \text{ O \% nm}$$

$$E_{aD} = 119.9 \text{ kJ/mol}$$

$$D_0 = 0.075 \text{ cm}^2/\text{s}$$

oxide dissolution

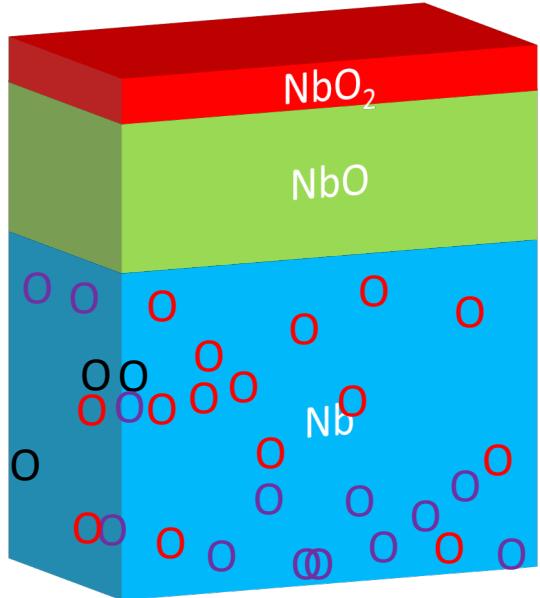
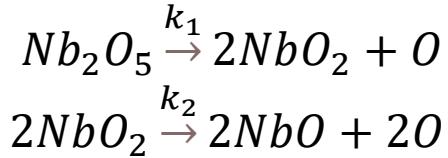
$$u_0 = 200 \text{ O \% nm}$$

$$E_{ak} = 131 \text{ kJ/mol}$$

$$A = 0.9 \times 10^9 \text{ l/s}$$

Model of oxide dissolution - Extension

$$-\frac{dA}{dt} = k_1 A; \quad -\frac{dB}{dt} = k_2 B - 2k_1 A; \quad -\frac{dC}{dt} = -k_2 B$$



$$A = A_0 \exp(-k_1 t)$$

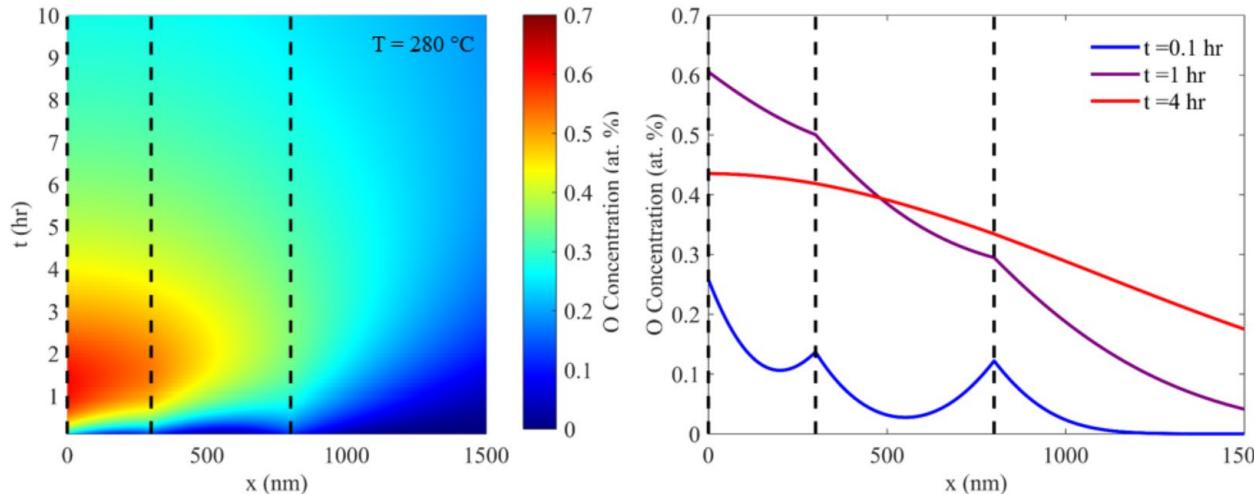
$$B = \frac{2A_0 k_1 (\exp(-k_1 t) - \exp(-k_2 t))}{k_2 - k_1} + B_0 \exp(-k_2 t)$$

$$C = 2A_0 \left(\frac{k_1 \exp(-k_2 t) - k_2 \exp(-k_1 t)}{k_2 - k_1} + 1 \right) + B_0 (1 - \exp(-k_2 t)) + C_0$$

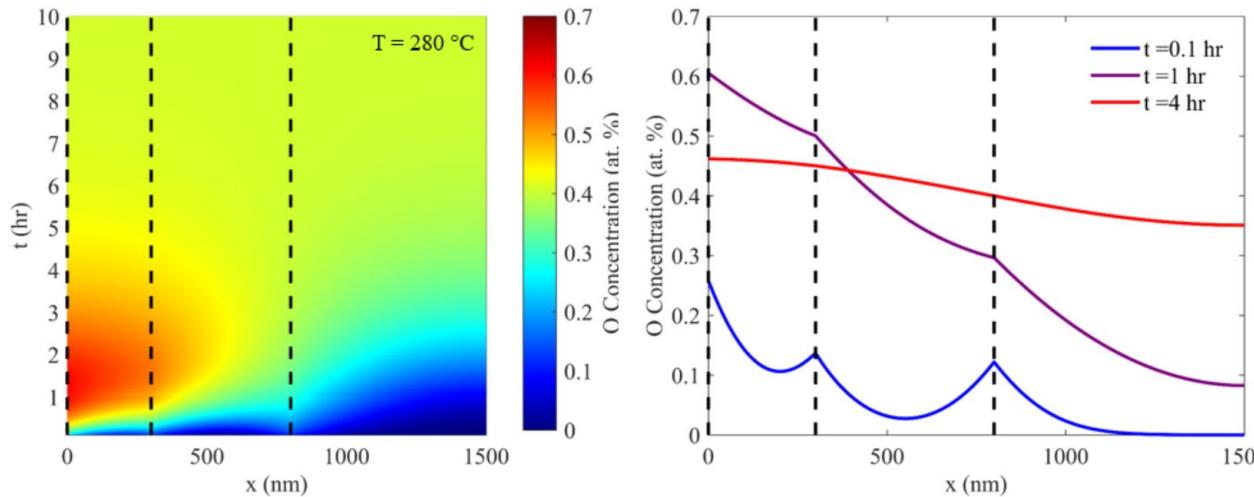
$$\frac{\partial c(x, t)}{\partial t} = D(T) \frac{\partial c(x, t)}{\partial x^2} + \sum q_x(x, t) \quad k_2 B \propto q_2(t)$$

Application to Arbitrary Sources in Semi-infinite Slabs and Films

Semi-infinite Slabs



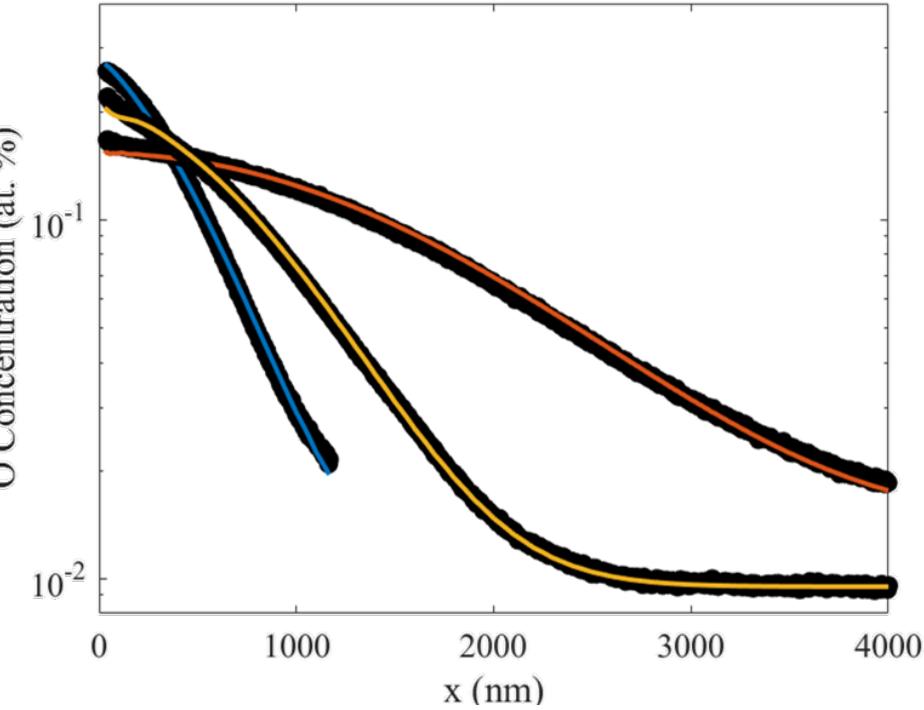
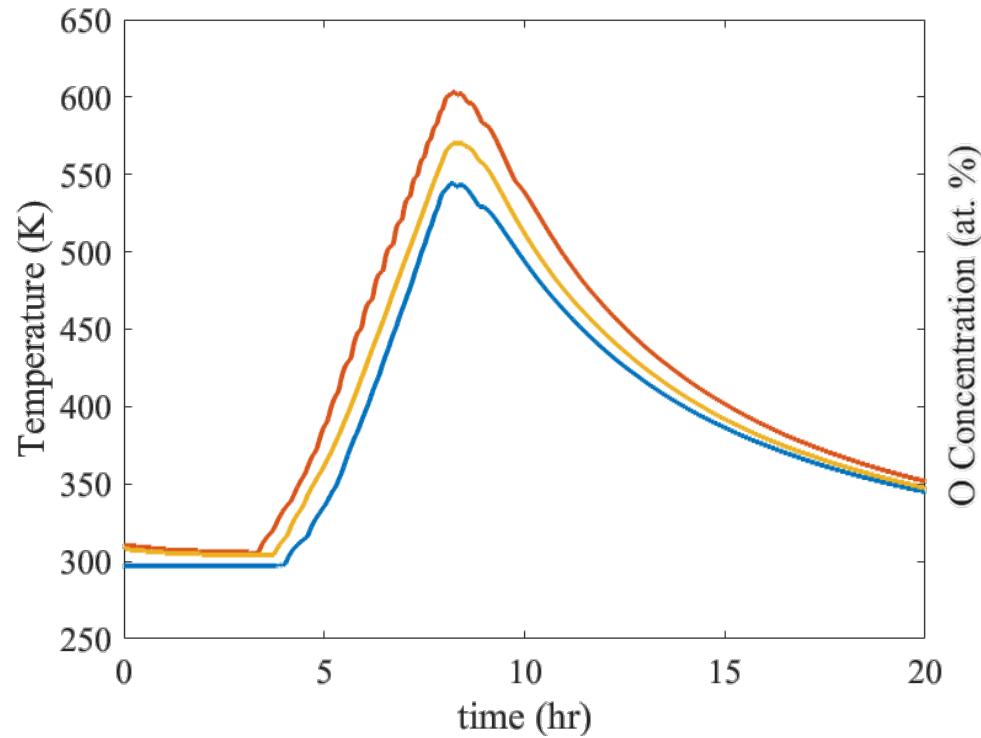
Films with O Diffusion Barrier



$$c(x, t) = \sum \frac{v_0}{\sqrt{(4\pi Dt)}} \left(\exp\left(-\frac{(x - a_n)^2}{(4Dt)}\right) + \exp\left(-\frac{(x + a_n)^2}{(4Dt)}\right) \right) + \int_0^t \frac{\gamma(s)}{\sqrt{(4\pi D(t-s))}} \left(\exp\left(-\frac{(x - a_n)^2}{(4D(t-s))}\right) + \exp\left(-\frac{(x + a_n)^2}{(4D(t-s))}\right) \right) ds + c_\infty$$

$$c(x, t) = \sum_{k=-\infty}^{\infty} \sum_{n=1}^m \frac{v_0}{\sqrt{(4\pi Dt)}} \left(\exp\left(-\frac{(x - a_n - 2kd)^2}{(4Dt)}\right) + \exp\left(-\frac{(x + a_n - 2kd)^2}{(4Dt)}\right) \right) + \int_0^t \frac{\gamma(s)}{\sqrt{(4\pi D(t-s))}} \left(\exp\left(-\frac{(x - a_n - 2kd)^2}{(4D(t-s))}\right) + \exp\left(-\frac{(x + a_n - 2kd)^2}{(4D(t-s))}\right) \right) ds + c_\infty .$$

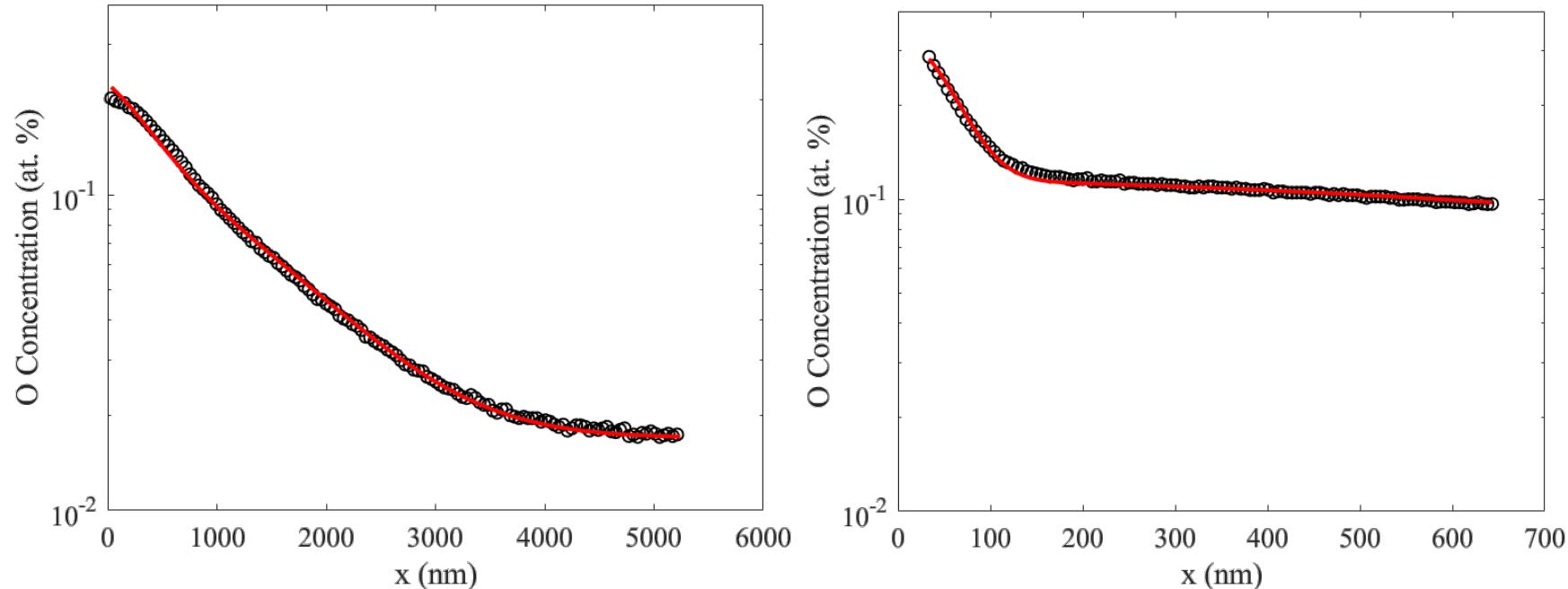
Short Heat Treatments



- Suppose you want to employ a short heat treatment at higher temperatures to promote greater oxide dissolution but keep a short diffusion profile. In this case heating and cooling steps may be relevant.

$$\begin{aligned}\frac{\partial c(x, t)}{\partial t} &= D(T(t)) \frac{\partial^2 c(x, t)}{\partial x^2} + q(t, T(t)) \\ -\frac{dA}{dt} \propto q &= u_0 k(T(t)) \exp\left(-\int_0^t k(T(s)) ds\right) \delta(x).\end{aligned}$$

Two-step Baking



1. Start with the input of Ciovati's model for the first temperature and time
2. Re-oxidize the surface
3. Replenish the sources in the model and advance the solution numerically.

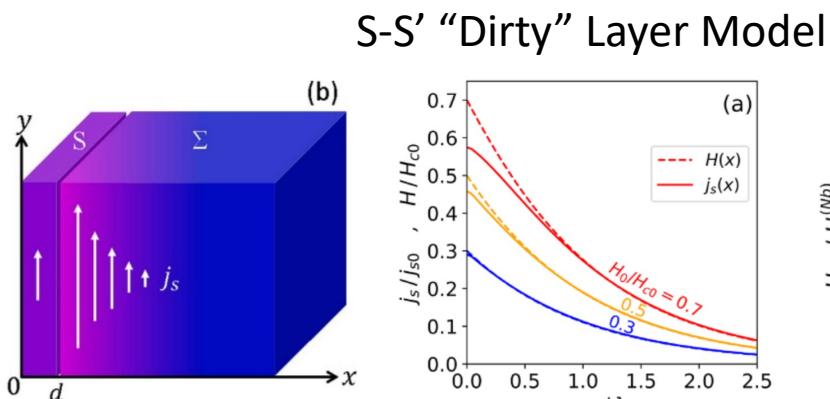
$$\frac{\partial c(x, t)}{\partial t} = D(T) \frac{\partial^2 c(x, t)}{\partial x^2} + q(t, T)$$

Outline

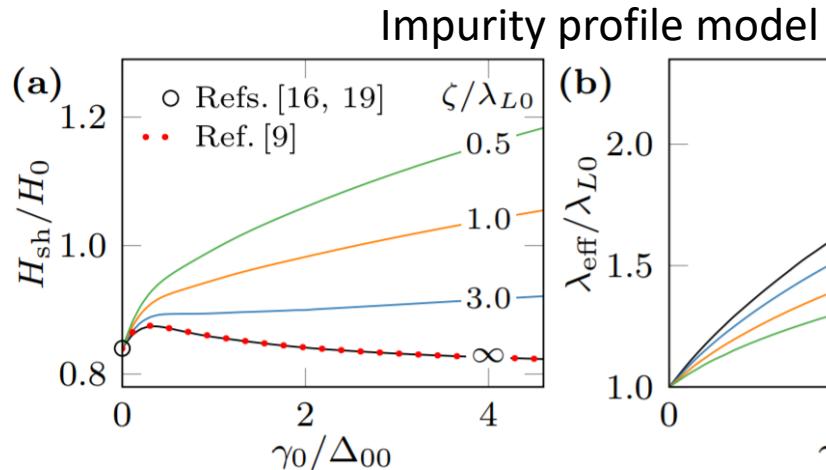
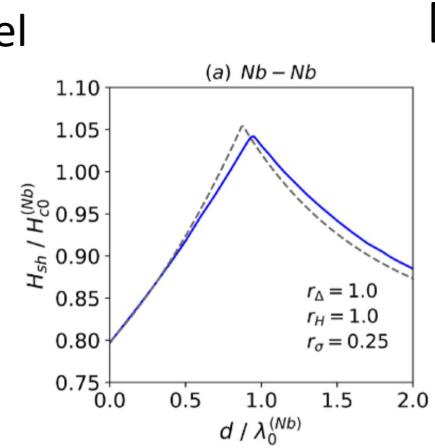
- Motivation
- Modeling O Diffusion
- Where next?

Where Next? – Shallow Impurity Profiles

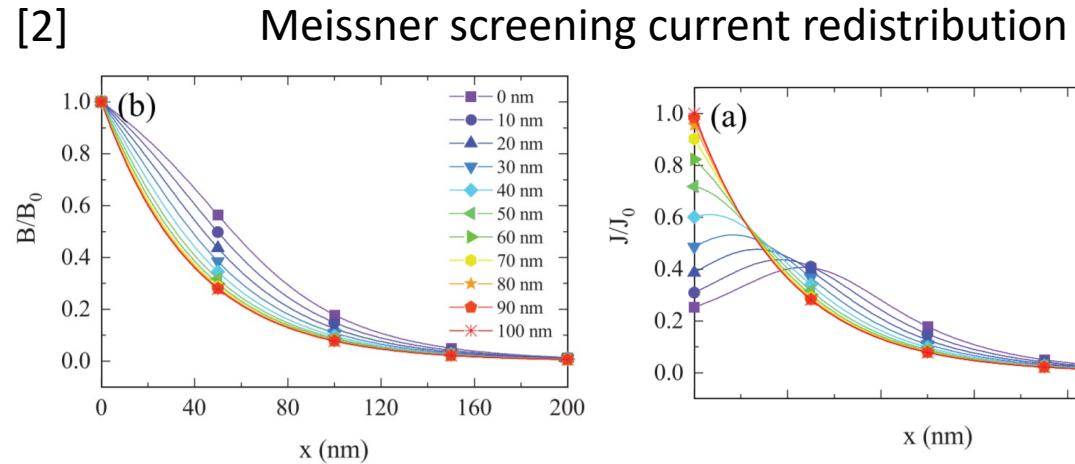
[1]



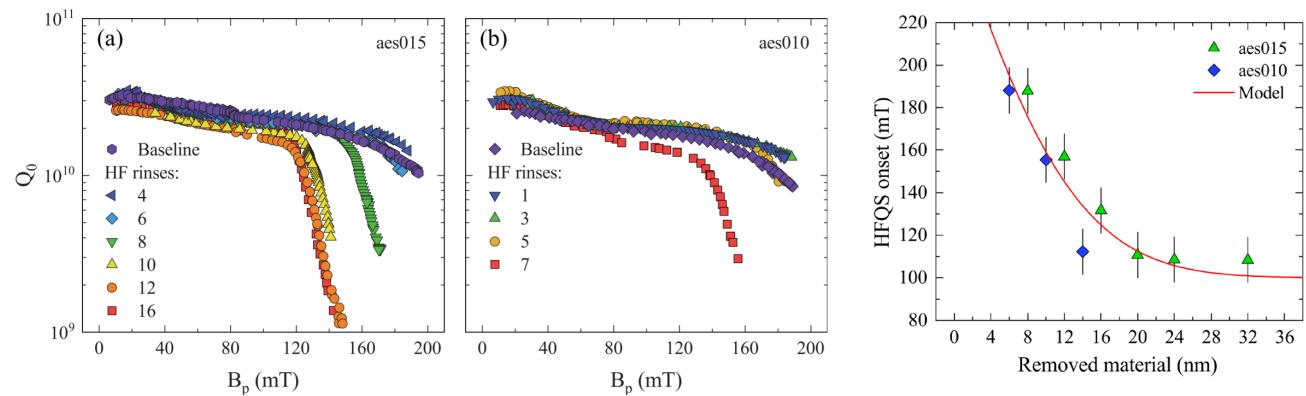
[3]



[2]



Reappearance of HFQS with HF rinses



- Many theoretical and experimental results suggest that shallow impurity profiles can be used to extend E_{\max}
- We are currently pursuing this using the oxide dissolution and oxygen diffusion model we have characterized
- Further characterization of Nb samples heat treated with only a temperature ramp to improve O diffusion modeling for short diffusion profiles

[1] T. Kubo *Superconductor Science and Technology* 34.4 (2021): 045006.

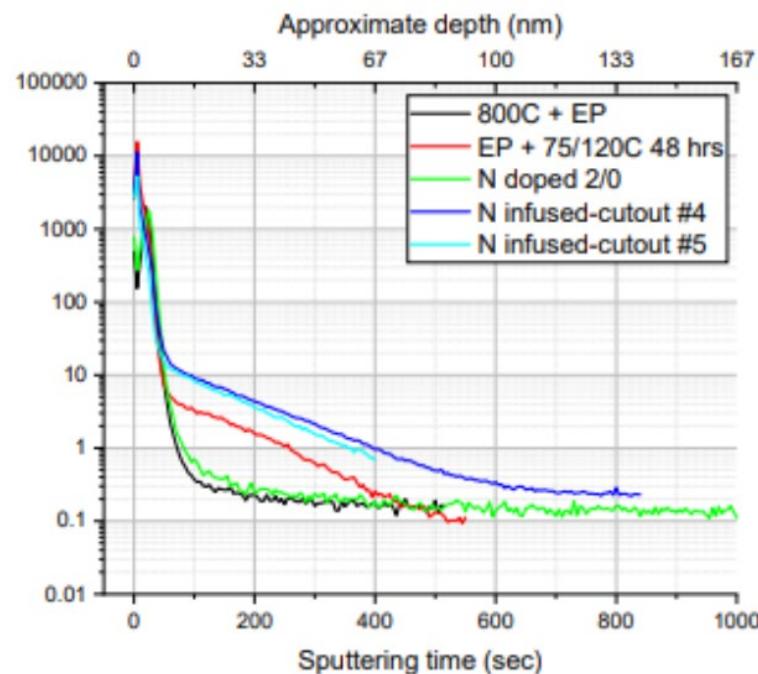
[2] M. Checchin and A. Grasselino *Appl. Phys. Lett.* 117, 032601 (2020)

[3] N. Vudtiwat, and J. A. Sauls. *Physical Review Research* 1.1 (2019): 012015.

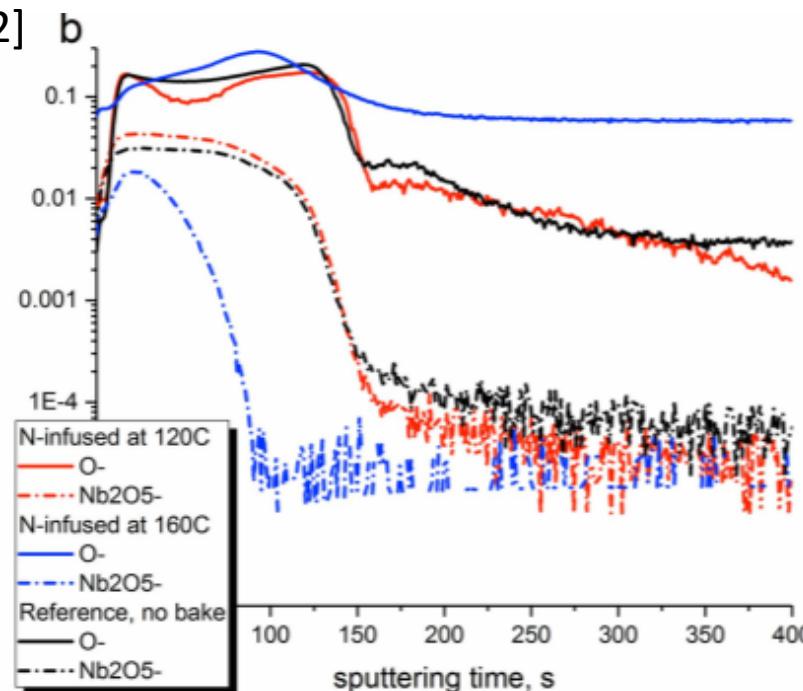
Role of Oxygen in Infusion Recipes

- SIMS measurements show that oxygen may be the dominant agent in “N-infused” cavities

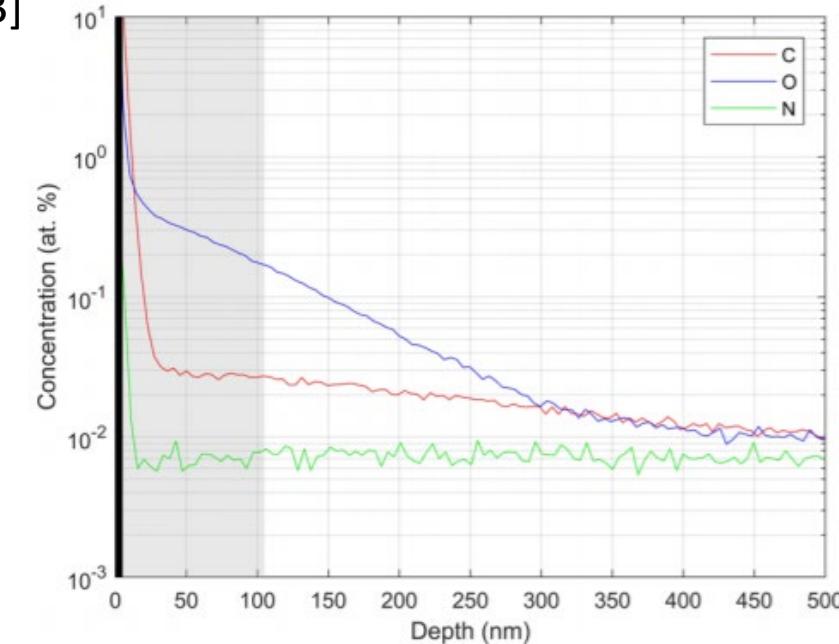
[1]



[2]



[3]



- If the infusion recipe is related to the impurity profile, can the impurity profile in “N-infused” cavities be engineered using only O and allow for a reproducible high Q_0 high, high E_{acc} cavity?

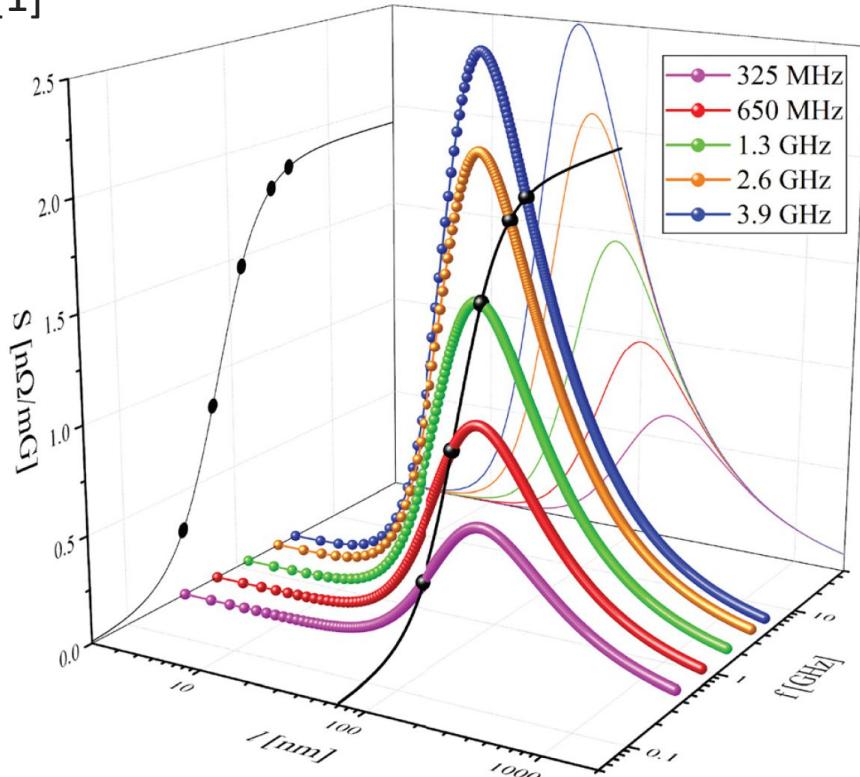
[1] A. Romanenko in *19th International Conference on RF Superconductivity* (JACoW, Dresden, 2019).

[2] A. Grassellino *et al.*, *Superconductor Science and Technology* **30**, 094004 (2017).

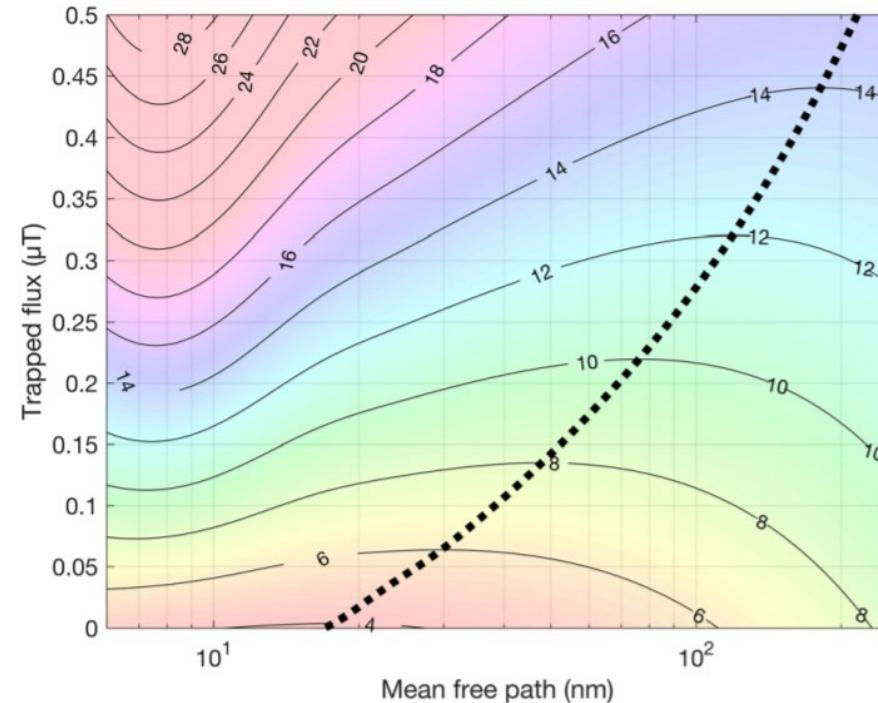
[3] J. Maniscalco, *et al.*, in *19th International Conference on RF Superconductivity* (JACoW, Dresden) Modeling O Diffusion During Nb Oxide Dissolution

Necessity for Impurity Tunability

[1]



[2]



- Sensitivity to trapped flux is frequency and mean free path dependent
- Depending on expected trapped flux, mean free path tunability is required!
- A deeper understanding of the native oxide dissolution and oxygen diffusion process can help guide precise alloying

Conclusions/Where Next?

Conclusions

- We've used SIMS to determine parameters in modeling the Nb pentoxide dissolution and O diffusion process.
- Extended Ciovati's model of native oxide dissolution for Nb which may be of use to other oxide dissolution processes.

Where next?

- Continue to explore the oxide dissolution parameter space with cavity test and SIMS analysis
- Explore the role of tailored impurity diffusion profiles within the RF penetration depth
- Explore multiple dissolutions or multi-step temperature profile
- Apply recipes to cavities with a more complex geometries

Acknowledgements

JLab
Ari Palczewski
Charlie Reece

Virginia Tech (SIMS)

Jonny Angle
Michael Kelley

NCSU
Fred Stevie

JLab Staff

Question Time...

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